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Automated Development of Manual Startup and Shutdown Procedures by a Non-linear Non-derivative Optimization Algorithm

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The most critical phases of plant operativity are the start-up and shutdown, which are usually implemented by following an experience-based sequential manual procedure. This work aims to develop an optimizing route for the unsteady states of a chemical plant through non-derivative local minimization algorithms. The proposed library for such development is NLopt, an open-source collection of optimization algorithms that can be implemented in C++ and Python languages. The definition of the problem followed a Monte Carlo initialization approach and optimization with a successive algorithm validation to test the optimizer potentiality. The case studies implemented describe common units in chemical plants and show the prospects of the route for the automation of such phases, in order to transform obsolete manual sequences into non-time-consuming and energy-saving routes to be implemented in plant activity.

1. Introduction

In the field of chemical engineering, the relevance of optimal operativity conditions is crucial, due to the high costs of the equipment, raw materials, and manual work; the safety concerns and regulations that must be followed to avoid dangerous situations, losses of money and operative time, energy consumption and environmental impact. Current applications focus on the steady phases of the process, leaving a big area for improvement in the study of dynamic situations. In particular, the study of the start-up and shutdown of a plant is a fundamental step to prevent machinery failure and guarantee plant productivity. Currently, in literature, many foci on the usage of control system theory approaches, such as model predictive control (Larsson et al., 2013), fuzzy control logic (Ali and Abu Khalaf, 2003) and hybrid control systems (Verwijs et al., 1995), which require high computational time due to the tuning requirement and complexity of the dynamic problem. This leaves a grey area for the development of optimized sequential procedures without the aid of control theory.

1.1 Problem's definition

The study focused on the development of an optimal routine for the time optimization of the start-up of chemical plants' standard units. An objective function f(x) was developed for each case study, translating physical and safety constraints into equality h(x) and inequality constraints g(x), following the standard for the optimization problem, reported in (1).

 $\min_{x_0,\ldots,x_n} f(x)$

h(x)=0

g(x)≤0

 $x=[x_1,x_2,...,x_n]$, $x_i \in \{0,100\}$

(1)

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2. Materials and methods

2.1 Case studies

Two chemical plants units were taken under study for the testing of the optimizer's capability to find convergence for time-discretized models.

2.2 Methods

The models of the units were based on mass and energy balances (2), and implemented as a set of differential equations over time to study the dynamics of the systems.

$$\sum \dot{m}_{i,in} - \sum \dot{m}_{i,out} + \dot{m}_{gen} = Acc.$$

$$\sum \left(\frac{1}{2}\dot{m} v^2 + \dot{m} gh + \dot{H}\right)_{i,in} - \sum \left(\frac{1}{2}\dot{m} v^2 + \dot{m} gh + \dot{H}\right)_{i,out} + \sum Q_j + \dot{W}_s = Acc \qquad (2)$$

The PDEs were simplified through the help of the *method of lines*, which allowed reducing them to a set of ODEs by discretizing one of the partial derivates by finite differences, as shown in the set of equations in (3).

$$\frac{\partial C_{i}}{\partial t} = -\frac{v_{0}\partial C_{i}}{\partial V} + r_{i}$$

$$\frac{\partial C}{\partial V} = \frac{C_{k+1} - C_{k}}{V_{k+1} - V_{k}} , \quad k=1,...,n$$
(3)

NLopt was chosen as the optimization tool, which is a free/open-source library for nonlinear optimization, providing one interface for several free optimization routines available online as well as original implementations of various other algorithms. It addresses general nonlinear optimization problems of the form (1). In order to feed an appropriate first guess to the optimizer, a Monte Carlo analysis was included. This technique relies on repeated random sampling to obtain numerical results (Kroese at al., 2014).



Figure 1 - Problem's definition block scheme

The algorithm's performance was then evaluated through a benchmark study, through accuracy and robustness results. It was carried out by providing a comparison between the capability of the algorithm to converge to a minimum, how fast this was achieved, and which one would overall seem best suited for the problem. In terms of computational time invested the algorithms were tested to reach the optimal value for the same number of iterations allowable from the optimizer, as well as testing the accuracy towards the minimum convergence.

2.3 Tools

As already stated, the problem was constructed in the high-level, general-purpose programming Python language, which provides a range class of free and open-source libraries. Between these, the SciPy was implemented for the differential system's resolution, both through the aid of the 'solve_ivp' function.

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NLopt was set up according to the library's requirements for algorithm choice, boundary conditions and tolerance for convergence, which are reported in Algorithm 1.

Algorithm 1 NLopt Optimization

- 1: initialization
- 2: opt.nlopt.opt(nlopt.algorithm, n_steps)
- 3: set lower bounds
- 4: set upper bounds
- 5: set minimization of the objective function
- 6: set of tolerance for the minimization
- 7: x = opt.optimize(initial guess)

3. Models

3.1 Atmospheric tank

The first case taken under study was the emptying of a tank, in which the variable is the opening of the valve for the fluid exiting the vessel. The unit was modelled through a mass balance to obtain the liquid's height profile over time. The velocity was expressed with Torricelli's law for a fluid exiting a recipient in a uniform gravitational field. In this case, the goal was to minimize the overall time of emptying the tank, so the set-point was the level of the liquid in the tank equal to zero. The solver was given a goal to minimize the total time invested in emptying through the objective function expressed in (5). The function is solved over the whole time domain, rather than at every time step the function is the sum of each integrating time step until the set point is met.

$$f(\mathbf{x}) = \sum_{i=0}^{SP \text{ fulfilment}} dt$$

(5)

3.2 Steam reforming reactor

The second case study regards the warm start-up of a steam reforming unit, based on a manual procedure obtained from a biogas real plant reacting unit, Figure 3. In this case, the unit was studied to provide an automated sequential procedure, in the scenario of which a new catalyst is to be inserted as packing material into the reforming tubes. The overall goal was still to successfully bring the system to nominal conditions with the least amount of time invested. This was to be carried out following a group of set points, obtained from the physical constraints applied to the system. The most relevant one regards the time required for the system to maintain the steady-state conditions, set to 10 minutes for the case study.

The case study's physical values were taken from previous work (Quirino et al., 2020), modelling the catalytic tubes inside the reformer as packed PFRs. The variables to be manipulated were the flow rates of water and methane fed to the steam reforming of the methane reactor, always through the percentage of valve opening. In this case, the approach that was taken involved a double optimization, to first find the optimal sequence to follow the precise procedure given, and an external optimization on the time interval upon which every controlled

variable could spend, allowing to find the same trajectory within a shorter time, the overall scheme of the objective function setup can be found in Figure 2. To develop such procedure, two objective functions where here taken into consideration, rather than the single one for the first case study; both are reported in Figure 2.



Figure 2 – Optimization route for the steam reformer case study

The first one stated as MSE (Minimum Squared Error), brings the system from the operating conditions to the required set points by minimizing the quadratic difference between the values of the methane and water flowrates (F_i) and the required flowrate values (F_{sp}).

Afterwards, the second optimization routine is recalled, working on optimizing the overall time taken by the system to meet nominal operating conditions, similar to the one used for the first case study.

Table 1 - Physical constraints of the system

Physical		Value	UoM
constraint			
S/C	3		-
F _{H2O} max	48		l/h
F _{CH4} max	25		Nm3/h

The physical constraints that allow optimal operativity and minimize risks are the steam-to-carbon ratio (S/C), for optimal productivity, and the maximum inlet flow rate's consumption, given from the piece of equipment, these were implemented as numerical constraints to feed to the solver, values are reported in Table 1.



Figure 3 - Startup of a reformer unit from real company procedure

4. Results and discussion

The results here discussed focus on the use of a non-derivative local minimum finding algorithm for the optimization of a non-linear objective function subject to linear constraints and its outcome.

The main focus of the first case study was on the testing of the library's capability to solve the problem of the minimum time of emptying is trivial to obtain with a full opening of the valve. Monte Carlo's results show already an initial guess very close to the solution. The optimizer tested successfully, in fact in

Figure 5b the profile of emptying matches the wanted solution. Some limits can be found in the profile's behaviour since once this had reached the set point required, the objective function isn't able to give further information to the system. The algorithms' comparison showed fast convergence for Powell's based methods, COBYLA (Powell, 1994) and BOBYQA (Powell, 2009) and bad performance for Brent's method PRAXIS (Richard, 2002). This brought to the conclusion that for this case the best compromise between all the aspects considered for the performance evaluation is the COBYLA algorithm.

For the second case study, a reference for the required set points to be followed during the start-up procedure was provided from a biogas facility. The procedure's profiles are reported in Figure 3. After the double optimization routine, the system shows good results in terms of total time spent by the system to reach the nominal operative conditions. The fundamental aspect to carry this optimization out was the decision of the constraints for the minimum time at which each set-point needed to be maintained.

In this case, the Monte Carlo initialization verges from the optimal trajectory, due to the presence of the multiple set-points, but with a high number of runs and time discretization intervals, the method still provided a good starting point for the optimization.

The algorithms behaviour was tested for the overall optimization of the two objective functions; having a limit within the library settings, the only algorithm to be able to receive equality and inequality constraints from the NLopt setup is the COBYLA, so to carry out the comparison between the class of algorithms the constraints had to be implemented within the objective function. Also, in this case, the BOBYQA and NEWOUA bound

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(Powell,2004) provided good convergence after a number of iterations benchmark. The tradeoff between accuracy, convergence and CPU time invested pointed at BOBYQA as the optimal algorithm for this problem.



Figure 4 - Algorithm's performance analysis a) convergence capability for maximum iterations allowed to the solver; b) total CPU time for each set run with respect to the maximum number of iterations



Figure 5 - Tank's optimization results a) Monte Carlo initialization profile compared to the ideal profile; b) Monte Carlo initialization valve openings; c) Optimal profile compared with the ideal one; d) Optimized valve opening

5. Conclusions

In conclusion, this study tried to provide a starting base for the study of optimization for unsteady phases of start-up and shutdown in industrial plants and their automation. The work provides an alternative approach to the obtaining of manual and sequential procedures currently followed by industrial companies, which require experimental knowledge for each unit. Through the aid of the open-source library NLopt, the algorithm is able to provide a sequence of action to bring the system close to nominal conditions.

The study has still room for further investigation, especially regarding the implementation of more complex process systems as well as the implementation of additional optimization tools, such as reinforcement learning algorithms, could be investigated.



Figure 6 - Optimized profiles for reformer start-up procedure a) Flowrates profile; b) Valve opening requirement

Nomenclature

- C_i ith component concentration, mol/m³
- g gravity acceleration, m/s²
- H enthalpy of the system, J
- h- height, m
- mi ith component mass flowrate, kg/s
- mgen generation term kg/s
- ODE ordinary differential equation

 r_i reaction rate, mol/m³/s Q – heat exchanged in the system, J PDE – partial differential equation PFR – plug flow reactor V – volume of the system, m³ v – velocity of the mass, m/s

- $W-work\ consumed\ by\ the\ system,\ J$

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